

### §13. Burning Criteria for D-<sup>3</sup>He Reactor

Nagayama, Y., Tomita, Y.

Burning criteria for a D-<sup>3</sup>He fusion reactor have been investigated by using the 0-D power and particle balance equations and the IPB98(y,2) scaling law [1]. In order to simplify the problem, ST configuration with ITB and the bootstrap current fraction of 100 % are assumed.

The model is as follows: Equations to be solved in this paper are the energy balance equation, as

$$\frac{dW}{dt} = P_{heat} - \frac{W}{\tau_E}$$

and the particle balance equations, as

$$\frac{dN_k}{dt} = v_k - \frac{N_k}{\tau_p} - \frac{1}{V} \sum_i S_{jk} + \frac{1}{V} \sum_{i+j \rightarrow k} S_{ij}$$

where  $W(t)$  is the internal plasma energy,  $N_k$  and  $v_k$  is the total particle number and the external particle supply of nucleus  $k$ , respectively. The summation indicated by  $i+j \rightarrow k$  is the whole fusion reaction creating a nucleus  $k$ , ( $i, j, k=H, T, D, {}^3\text{He}, C$ ). The electron density  $n_e$  and the ion density  $n_i$  satisfy the charge neutrality. The energy confinement time  $\tau_E$  is assumed to be  $\gamma_{HH}$  times of the IPB98(y,2) scaling. Spatial profiles of the temperature and density are assumed to be an ITB model as  $T_j(r) = T_{j0} g(x; b_T, m_T)$  and  $n_j(r) = n_{j0} g(x; b_n, m_n)$ . Here  $x=r/a$ , and

$$g(x; b, m) = \begin{cases} 1 - \frac{x^{2m}}{b^{2(m-1)}} & (0 \leq x \leq b) \\ \frac{(1-x^2)^m}{(1-b^2)^{m-1}} & (b \leq x \leq 1) \end{cases}$$

Figure 1 shows the  $T_i/T_e$  and the fraction of neutron power in the total fusion power versus the <sup>3</sup>He in the case of  $R=6$  m. When  $T_i=T_e$ ,  $n_D: n_{{}^3\text{He}}=2:1$  and the neutron fraction is 10 %, which is 1/8 of the D-T reactor. When  $n_{{}^3\text{He}}=60$  %, the neutron fraction is 1.9 % of the total fusion power, which is less than 1/40 of the D-T fusion. The  $T_i/T_e$  should be greater than 2 in order to operate the reactor with  $n_{{}^3\text{He}}=60$  % even if no impurity other than fusion ashes (H and <sup>4</sup>He)

exists in plasma. D-D reactor or a low-neutron D-<sup>3</sup>He reactor require the condition  $T_i/T_e > 2$  even if no impurity other than the <sup>4</sup>He ash remains.

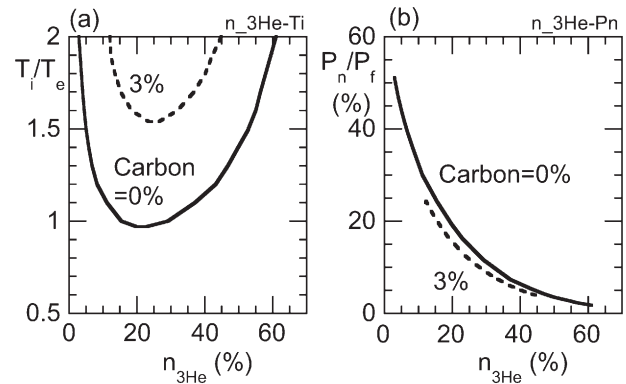


Fig. 1 (a) Temperature ratio ( $T_i/T_e$ ) and (b) fraction of neutron power in total fusion power versus <sup>3</sup>He contamination in the steady burning state.

Figure 2(a) shows the minimum toroidal field ( $B_t$ ) to obtain a particular central beta ( $\beta_0$ ). Fig.2 (b) shows the averaged beta ( $\langle\beta\rangle$ ) versus normalized radius of ITB foot point ( $b_{ITB}$ ) in the case of,  $B_{coil}=20$  T ( $B_t=3.63$  T) and  $\beta_0=1$ . Other conditions ( $R=6$  m,  $T_i/T_e=1.6$ ,  $n_D: n_{{}^3\text{He}}=2:1$  and  $n_C=3$  %) are common in both figures.

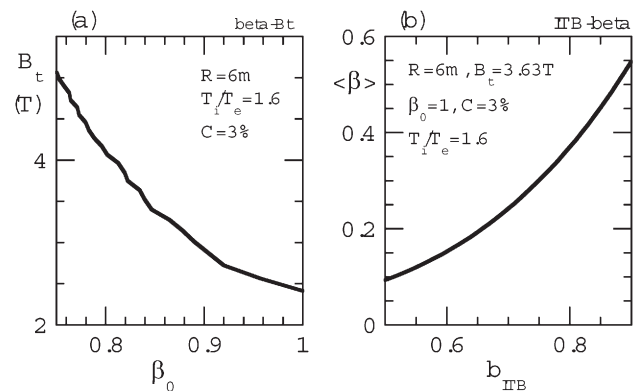


Fig. 2 (a) Required  $B_t$  to obtain  $\beta_0$  in the case of  $b_{ITB}=0.85$ . (b) Averaged beta ( $\langle\beta\rangle$ ) versus  $b_{ITB}$ .

The result shows that when  $\langle\beta\rangle=10$  %, D-<sup>3</sup>He reactor is possible if  $\beta_0$  is about unity and  $T_i/T_e>2$ . This is applicable to helical reactors.

- [1] Y. Nagayama, Y. Tomita, IEEJ Trans. FM, Vol.125, 947 (2005)